

1 **Video-based analysis of head-torso coupling during lateral impacts under passive and co-contracted**
2 **conditions**

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10 Keywords: Head-torso coupling·Kinematic response·Video-based motion analysis·Muscle activation

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14
15 Clinical trial number: not applicable.

16

17 Abstract word count: 235

18 Manuscript word count: 5,715

19 Figures: 6

20 Tables: 3

21

22

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28 **Abstract**

29 **Purpose** Current surrogate necks and computational models lack empirical data on in vivo head-torso
30 coupling across muscle activation states, limiting their biofidelity during impact testing. This study
31 quantified head and torso kinematics and head-torso coupling during controlled lateral impacts under
32 passive and co-contracted cervical muscle conditions.

33 **Methods** We conducted a secondary video analysis of high-speed footage (500 Hz) from Reynier et al.
34 (2020), tracking frame-by-frame head and torso motion in 19 male participants during standardized lateral
35 impacts (3.7 kg padded impactor at 2.0 m/s). Participants experienced impacts under passive (relaxed) and
36 maximally co-contracted muscle conditions. Outcome measures included peak displacement, path length,
37 head-torso relative excursion, velocity time lag, and peak linear kinematics.

38 **Results** Co-contraction reduced peak head displacement by 30% (14.2 ± 3.4 cm to 10.0 ± 3.6 cm, $p < 0.001$,
39 $d = -1.51$) and path length by 21% ($p < 0.001$), with all 19 participants showing displacement reductions.
40 Head-torso relative excursion decreased by 36% (11.3 ± 3.3 cm to 7.2 ± 3.2 cm, $p < 0.001$, $d = -1.35$), and
41 velocity time lag shortened from 88 to 66 ms ($p = 0.002$). Peak linear acceleration remained unchanged
42 (10.3 ± 0.9 g vs. 10.1 ± 1.0 g, $p = 0.415$), while peak head velocity decreased by 6% ($p = 0.003$). Peak
43 angular velocity and angular acceleration also remained unchanged ($p = 0.320$ and $p = 0.820$).

44 **Conclusion** Cervical muscle co-contraction reduces head displacement by mechanically coupling the head
45 to the torso, constraining displacement and velocity without altering peak acceleration or angular
46 kinematics. These coupling metrics provide validation targets for surrogate neck designs and computational
47 head-neck models incorporating active musculature.

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50 **Introduction**

51 Inaccurate surrogate neck designs compromise our ability to predict and prevent traumatic brain injury.
52 Sports-related concussions affect an estimated 1.4 to 3.8 million athletes annually in the United States [1,
53 2]. Reducing these injuries requires accurate laboratory testing with surrogates that replicate human
54 biomechanics. Current anthropomorphic test devices (ATDs) and human body models (HBMs) lack
55 empirical data on head-torso coupling needed to replicate human neck mechanics during impacts [3, 4].
56 This gap compromises safety testing across sports and automotive applications. This study addresses that
57 gap through simultaneous measurement of both segments.

58 Peak acceleration provides an incomplete picture of the kinematic environment that causes brain injury.
59 Brain tissue strain depends on spatial displacement and rotational velocity throughout the impact, not
60 instantaneous acceleration maxima [5, 6]. Accelerometers measure motion at discrete anatomical locations
61 but miss relative displacement between body segments [7–9]. Angular acceleration generates shear strains
62 within brain tissue, causing diffuse axonal injury even without skull fracture [7, 8]. Spatial displacement
63 and rotational kinematics predict concussion risk more accurately than peak linear acceleration alone [9].

64 Head-torso coupling determines head displacement during impact as much as impact severity itself. The
65 torso anchors the system, and coupling strength dictates whether the head moves independently or as part
66 of a larger linked mass. Researchers have measured head-to-torso kinematics during rear-end whiplash
67 impacts and soccer heading, but these loading conditions differ from the direct lateral impacts common in
68 contact sports [10, 11] and lateral automobile collisions. Quantifying coupling during lateral head impacts
69 requires simultaneous measurement of both segments throughout the impact sequence.

70 Head-torso coupling modulates the head's kinematic response by changing its effective mass. When the
71 head moves independently, impact forces accelerate only the isolated head mass (~4.5 kg). Active muscle
72 co-contraction mechanically couples the head to the torso, engaging additional body mass and reducing

73 head kinematic response [12]. Video reconstruction of NFL helmet collisions demonstrated this principle:
74 striking players who aligned head, neck, and torso before impact transferred momentum through the linked
75 segment, while struck players whose heads moved independently experienced greater accelerations [12,
76 13]. Laboratory studies confirm that greater neck strength and anticipatory muscle activation reduce peak
77 linear and angular velocity after impulsive loading [14, 15]. Coupling provides this protective effect by
78 distributing impact energy across a larger effective mass rather than by reducing peak contact forces.

79 The degree of head-torso coupling may influence injury risk independently of peak acceleration, though
80 computational models indicate this effect diminishes at higher severities where muscular forces become
81 negligible [16, 17]. Despite this limitation, cervical muscle activation represents the most readily modifiable
82 parameter influencing coupling at sub-catastrophic impact levels. Athletes achieve neuromuscular
83 adaptations through training spanning weeks, whereas helmet designs or rule modifications require
84 extended development [18, 19]. No previous study has directly measured head-torso coupling through
85 simultaneous tracking of both segments in living humans.

86 Surrogate neck developers require empirical coupling data to address design limitations. The Hybrid III
87 neck assembly, the current standard for automotive and sports equipment testing, demonstrates these design
88 shortcomings. Its quasi-static bending stiffness exceeds that of a relaxed human neck by a factor of three
89 yet represents only one-third the stiffness of a tensed neck [20]. Its developers validated it only for sagittal
90 plane motion, and it performs poorly in lateral bending [21, 22]. No existing surrogate modulates
91 mechanical properties based on muscle activation state. Researchers adopt a single intermediate stiffness
92 that represents neither the passive nor the actively braced human neck [3]. Validating new biofidelic designs
93 requires *in vivo* data showing how segment coupling changes across muscle activation conditions [23, 24].

94 Quantifying head-torso coupling requires simultaneous tracking of both segments in a common reference
95 frame. Accelerometers require double integration to obtain position, introducing drift errors. Video tracking

96 with fiducial markers measures positions directly, achieving average errors of 1-1.5 mm during football
97 head impacts [25]. Integrated position signals outperformed peak acceleration for characterizing impact
98 kinematics in football players [26]. Direct position measurement avoids error accumulation while providing
99 spatial trajectory information. High-speed video systems can track multiple markers simultaneously,
100 enabling reconstruction of body segment motion throughout impact sequences [27].

101 We conducted a secondary video analysis to simultaneously measure head and torso kinematics during
102 controlled lateral head impacts. We processed high-speed footage from Reynier et al. (2020) to track both
103 segments in 19 participants during non-injurious impacts (3.7 kg padded impactor at 2 m/s) under passive
104 and co-contracted conditions. We reconstructed segment trajectories and quantified head-torso coupling
105 throughout the impact sequence. We hypothesized that cervical co-contraction reduces head displacement
106 relative to the torso by increasing mechanical coupling between segments. These data provide the *in vivo*
107 validation targets needed to develop more biofidelic surrogate necks and human body models.

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109 **Materials and Methods**

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111 **Study design**

112 We quantified head-torso coupling by analyzing high-speed video footage from controlled human head
113 impact experiments. We conducted a secondary analysis of video recordings from Reynier et al. (2020),
114 who delivered standardized lateral impacts to human volunteers under passive and co-contracted muscle
115 conditions. Our analysis extracted frame-by-frame positional data for both head and torso segments
116 throughout each impact, extending beyond Reynier's original focus on head-only kinematics measured via
117 instrumented mouthpieces. We tracked complete movement trajectories to quantify how muscle activation
118 alters the mechanical coupling between head and torso during non-injurious impacts.

119 **Participants**

120 The original study enrolled 20 healthy male volunteers. The mean participant age was 22.8 ± 3.0 years,
121 height was 177.4 ± 3.5 cm, and body mass was 78.2 ± 9.5 kg. Reynier et al. excluded individuals with any
122 history of concussion, neurological conditions, or recent musculoskeletal injuries. All participants provided
123 written informed consent for both the original data collection and future secondary analyses. The University
124 of Virginia Institutional Review Board for Health Sciences Research approved the original experimental
125 protocol (IRB-HSR #20486, "Non-Injurious Head Motion in Human Subjects," Principal Investigator: M.B.
126 Panzer). We obtained and used video recordings for 19 of the original 20 participants for this secondary
127 analysis.

128 **Experimental impact protocol**

129 A pendulum system delivered standardized lateral impacts to each participant's head. The pendulum
130 consisted of a 3.7 kg padded impactor covered with 6.35 mm polyurethane foam, suspended by two wires
131 to ensure consistent impact trajectory [28]. This design delivered impacts at a standardized location 75 mm
132 above the right tragus at 2.0 m/s velocity (Figure 1). A burned restraining filament released the pendulum
133 for each trial, ensuring precise timing control. Participants wore an additional 19.05 mm foam pad secured
134 by a swimming cap to standardize impact conditions and protect against injury (Reynier et al. 2020).

135 We tested two distinct muscle activation conditions to evaluate cervical muscle engagement effects on
136 impact response. The passive condition delivered impacts within a randomized 20-second window without
137 any countdown or warning, preventing anticipatory muscle activation. Surface electromyography
138 confirmed minimal sternocleidomastoid activation during the passive condition. The co-contracted
139 condition provided participants with a 3-second countdown before impact, during which they maximally
140 contracted their bilateral neck muscles following standardized instructions. All participants completed the
141 passive condition trials first to preserve the element of surprise and prevent learned anticipatory responses.

165 landmarks (buttons, seams) or anatomical references (supraclavicular notch, upper trapezius contour). The
166 absence of a standardized torso marker meant that tracking point locations varied between participants.
167 During digitization, the operator qualitatively evaluated each trial for marker motion relative to the
168 underlying anatomy and observed minimal marker-tissue artifacts across all trials. All 38 trials (19
169 participants \times 2 conditions) met quality standards for marker visibility and landmark identification. We
170 tracked both head and torso points in the medial-lateral (Y-axis, impact direction) and superior-inferior (Z-
171 axis) planes throughout each sequence. A single trained operator digitized all trials to maintain consistency.
172 Because each participant served as their own control, any systematic digitization bias affected both
173 conditions equally and cannot explain the within-subject differences we report.

174 **Signal processing and kinematic calculations**

175 We processed position data through a standardized filtering and synchronization pipeline before calculating
176 kinematic variables. We applied a fourth-order Butterworth low-pass filter with 50 Hz cutoff frequency
177 using zero-phase filtering, selected to preserve the primary kinematic content while attenuating digitization
178 noise. We derived velocity and acceleration using central differences for interior points and single-sided
179 differences at endpoints. We smoothed the resultant acceleration time series with a 3-point moving average
180 to reduce high-frequency noise amplified by double differentiation. We synchronized all trials to movement
181 onset ($t = 0$), defined as head resultant velocity first exceeding 30 cm/s. This threshold exceeded baseline
182 noise (5.0 ± 1.0 cm/s) by six standard deviations, ensuring reliable onset detection. We extracted data from
183 -50 ms to 500 ms relative to movement onset.

184 We calculated kinematic variables to quantify instantaneous motion, cumulative displacement, and head-
185 torso coupling (see Table 1 for details). Linear kinematics include peak resultant velocity and acceleration.
186 We calculated head angular velocity using the torso position at movement onset as the pivot point,
187 representing head rotation about the base of the neck. We calculated angular acceleration as the time
188 derivative of angular velocity and applied a fourth-order Butterworth filter at 50 Hz to both angular

212 spatial trajectory patterns for four representative participants to illustrate the spatial information that video
213 tracking provides; the Appendix contains complete trajectory data for all participants. We performed all
214 analyses in MATLAB R2024b (MathWorks, Natick, MA) and report means \pm standard deviations with
215 95% confidence intervals.

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262 **Discussion**

263 Cervical muscle co-contraction reduced head displacement by 30% and head-torso relative excursion by
264 36% while leaving peak linear acceleration unchanged. These findings indicate that bracing constrains head
265 displacement and velocity rather than reducing peak acceleration. Video-based tracking of both segments
266 enabled direct measurement of coupling dynamics throughout the impact sequence.

267 The results support the hypothesis that cervical muscle activation reduces head displacement through
268 increased head-torso coupling. Co-contraction decreased both relative excursion and time lag between
269 segments. Both head and torso displacement showed slopes of 0.70 relating passive to co-contracted values
270 (Figure 3), indicating proportional constraint regardless of baseline displacement. This pattern suggests the
271 head and torso moved as a more unified system. Finite element models support this mechanism, showing
272 that active neck muscle force increases acceleration and velocity coupling between head and T1 through
273 altered force transmission at the cervical spine [29]. NFL video reconstructions show similar effects, where
274 players who braced before contact experienced reduced head displacement compared to unaware players
275 [12, 13]. These trajectory changes matter for injury prediction because rotational kinematics and spatial
276 displacement predict concussion risk more accurately than peak linear acceleration alone [30, 31]. The
277 observed 6% reduction in peak head velocity reinforces the protective role of muscle activation beyond
278 displacement constraint alone. Cervical bracing provides protection by constraining head trajectory and
279 attenuating velocity, though these effects may diminish at higher impact severities where muscular forces
280 become small relative to impact forces [16, 17].

281 The differential effects of co-contraction on displacement, velocity, and acceleration have implications for
282 surrogate design. Current anthropomorphic test devices cannot capture the coupling changes we observed.
283 The Hybrid III neck operates at a single intermediate stiffness representing neither the passive nor actively
284 braced human neck. Both Hybrid III and Q-series ATDs produce reduced head rotation and neck excursions

285 compared to human volunteers due to rigid thoracic spine design [32]. Variable neck properties are
286 technically feasible, as THOR-NT muscle cables significantly stiffen neck response by reducing occipital
287 condyle joint laxity [22]. Cadaveric testing cannot provide these validation data because cadavers lack
288 active muscle response. Our displacement, velocity, and coupling metrics define the response envelope that
289 biofidelic surrogates must replicate.

290 Three factors limit the generalizability of our findings. First, we analyzed male participants experiencing
291 lateral impacts at a single severity, preventing conclusions about sex differences, impact direction effects,
292 and velocity-dependent responses. Second, manual video digitization captures position with lower temporal
293 resolution (500 Hz) than direct sensor measurement (10,000 Hz). Our video-based surface tracking shares
294 limitations with skin-mounted sensors that over-predict kinematics [27]. Torso tracking presented
295 additional challenges because Reynier et al. (2020) did not record the original footage for motion tracking
296 purposes. Variability in visible anatomical landmarks contributed to substantial inter-subject differences in
297 torso measurements ($CV = 56\%$ for torso acceleration) [28]. This variability does not undermine our
298 primary conclusions because head-torso relative excursion showed consistent large effect sizes ($d = -1.35$
299 to -1.67). The paired within-subject design ensures that digitization characteristics remain constant across
300 conditions for each participant, isolating muscle activation effects from measurement variability.

301 These methodological differences caution against direct comparison with Reynier et al. (2020), who
302 measured at the head center of mass using instrumented mouthguards. Despite these differences, both
303 approaches found unchanged peak acceleration between muscle conditions, reinforcing this finding's
304 robustness. Third, our protocol examined only two discrete muscle activation states, whereas athletes
305 continuously adjust cervical posture and activation patterns before contact [15].

306 Future research should prioritize testing female participants to establish sex-specific coupling mechanics,
307 given documented differences in neck strength and head-neck anthropometry [14, 19]. EMG-controlled

308 protocols can quantify graded muscle activation levels rather than discrete states. Examining multiple
309 impact velocities and directions will establish how coupling effectiveness varies across the biomechanical
310 range athletes experience. Cervical spine kinematics vary continuously during active movement, with
311 alignment and stiffness changing dynamically with position and direction [33–35].

312 Advances in computer vision offer opportunities to improve tracking precision while reducing operator-
313 dependent variability. Markerless pose estimation frameworks such as DeepLabCut and OpenPose now
314 achieve near-expert labeling accuracy with minimal training data [36–38] and have transformed movement
315 analysis in clinical gait assessment and sports performance [39]. Applying similar approaches to impact
316 biomechanics could expand tracking to full-body kinematic chains and extract data from existing video
317 archives.

318 In conclusion, anticipatory muscle activation reduced head displacement through increased head-torso
319 coupling in our sample of healthy male participants. Co-contraction constrained displacement, reduced
320 relative excursion, and attenuated peak head velocity while leaving peak acceleration unchanged.
321 Unanticipated impacts with relaxed musculature may place athletes at greater risk by allowing larger head
322 excursions during contact. These coupling data provide empirical targets for developing anthropomorphic
323 test devices and validating computational models with active cervical musculature. Replication with female
324 participants and across higher severities remains an important next step.

325

326 **Ethics approval.** The original experimental protocol was approved by the University of Virginia
327 Institutional Review Board for Health Sciences Research (IRB-HSR #20486, approved March 20, 2018).
328 The present study is a secondary analysis of video recordings collected under that approved protocol.

329
330 **Consent to participate.** All participants provided written informed consent (approved March 12, 2018) for
331 both the original data collection and future secondary analyses. The consent process included viewing a
332 video demonstrating the head impact procedure prior to enrollment.

333
334 **Consent for publication.** Participants consented to use of video recordings for research purposes. Raw
335 footage is not published due to participant identifiability. All published figures use de-identified trajectory
336 data or images of an anthropomorphic test dummy.

337 **Acknowledgements** We thank all participants who volunteered for the original study. We also thank the
338 Center for Applied Biomechanics at the University of Virginia for providing access to the high-speed video
339 footage from Reynier et al. (2020).

340 **Author Contributions.** P.K.: Conceptualization, Methodology, Formal analysis, Investigation, Data
341 curation, Visualization, Writing -- original draft, Writing -- review & editing. G.B.: Conceptualization,
342 Video Analysis, Investigation, Data curation, Formal analysis, Writing -- review & editing. K.R.:
343 Resources, Writing -- review & editing, Supervision (original data collection). M.P.: Resources, Writing -
344 - review & editing, Supervision, Funding acquisition (original study). P.C.: Conceptualization,
345 Methodology, Writing -- review & editing, Supervision, Project administration, Funding acquisition.

346 **Competing interests.** The authors declare no competing or financial interests.

347

348 **Funding.** This secondary analysis received support from the Natural Sciences and Engineering Research
349 Council of Canada (NSERC). The original experimental data collection reported in Reynier et al. (2020)
350 was supported by Football Research, Inc.

351

352 **Data availability.** Analysis code and processed kinematic summary data are publicly available at
353 <https://github.com/pkudzia/Paper---Head-torso-coupling>. Individual participant position coordinates,
354 velocities, accelerations, and displacement time series are available from the corresponding author upon
355 reasonable request. Raw video footage requires approval from the University of Virginia IRB (IRB-HSR
356 #20486) due to participant identifiability.

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457 21:7315, 2021.
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459

460 **Table 1.** Kinematic variable definitions and formulas. All variables derived from two-dimensional position
 461 data in the frontal plane (Y = medial-lateral, impact direction; Z = superior-inferior), normalized to
 462 movement onset. Categories include linear and angular kinematics, displacement metrics at peak and fixed
 463 time points (100 ms and 200 ms post-onset), and coupling metrics describing head motion relative to torso.
 464 For angular kinematics, y and z represent head position relative to torso position.

Variable	Units	Definition	Calculation Formula
Linear Kinematics			
Resultant Velocity	cm/s	Resultant linear velocity of head or torso, where v_y and v_z are velocity components in the medial-lateral and superior-inferior directions	$\sqrt{(v_y^2 + v_z^2)}$
Resultant Acceleration	g	Resultant linear acceleration of head or torso, where a_y and a_z are acceleration components in the medial-lateral and superior-inferior directions and g is the acceleration due to gravity.	$\sqrt{(a_y^2 + a_z^2)} / g$
Angular Kinematics			
Head Angular Velocity (ω)	rad/s	Angular velocity of head about torso, where y and z are head position relative to instantaneous torso position, and v_y and v_z are head velocity components	$(y \cdot v_z - z \cdot v_y) / (y^2 + z^2)$
Head Angular Acceleration (α)	rad/s ²	Angular acceleration of head, computed as time derivative of angular velocity	$d\omega/dt$
Displacement Metrics			
Peak Displacement	cm	Maximum straight-line distance from initial position, where y_0 and z_0 are initial coordinates	$\sqrt{((y-y_0)^2 + (z-z_0)^2)}$
Displacement at Time t	cm	Displacement at specified time post-onset (e.g., 100 ms, 200 ms), where y_t and z_t are coordinates at time t	$\sqrt{((y_t-y_0)^2 + (z_t-z_0)^2)}$
Path Length	cm	Total distance traveled during first 500 ms post-impact, summed across consecutive frames	$\Sigma \sqrt{((y_{i+1}-y_i)^2 + (z_{i+1}-z_i)^2)}$
Coupling Metrics			
Head-Torso Relative Excursion	cm	Change in head position relative to torso from onset, where $y_{rel}(t) = y_{head}(t) - y_{torso}(t)$ and $z_{rel}(t) = z_{head}(t) - z_{torso}(t)$	$\sqrt{((y_{rel}(t) - y_{rel}(0))^2 + (z_{rel}(t) - z_{rel}(0))^2)}$
Time Lag	ms	Temporal difference between head and torso peak values for a given metric	$t(\text{head peak}) - t(\text{torso peak})$

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467 **Table 2.** Displacement and coupling metrics for passive and co-contracted conditions (n = 19). Values are
 468 mean ± SD [95% CI]. Time lag = t(head peak) – t(torso peak); negative values indicate the head peaked
 469 first (acceleration, velocity), positive values indicate the head peaked after the torso (displacement). Δ% =
 470 percent change from passive to co-contracted. Paired t-tests; Cohen's d effect size.

Parameter	Passive	Co-contraction	Δ%	p	d
Head Path					
Peak Displacement (cm)	14.22 ± 3.44 [12.57, 15.88]	9.96 ± 3.57 [8.24, 11.68]	-30.0%	<0.001	-1.51
Time to Peak Displacement (ms)	271 ± 56 [244, 298]	220 ± 95 [174, 266]	-18.8%	0.004	-0.77
Displacement at 100ms (cm)	9.97 ± 1.36 [9.32, 10.63]	7.37 ± 1.20 [6.80, 7.95]	-26.1%	<0.001	-1.82
Displacement at 200ms (cm)	12.94 ± 2.39 [11.79, 14.09]	8.94 ± 2.58 [7.70, 10.19]	-30.9%	<0.001	-1.89
Path Length (cm)	19.07 ± 3.18 [17.53, 20.60]	15.02 ± 2.48 [13.83, 16.21]	-21.2%	<0.001	-1.66
Torso Path					
Peak Displacement (cm)	3.73 ± 0.99 [3.26, 4.21]	3.37 ± 0.90 [2.94, 3.81]	-9.7%	0.026	-0.56
Time to Peak Displacement (ms)	199 ± 42 [179, 219]	171 ± 49 [148, 195]	-13.9%	0.024	-0.57
Displacement at 100ms (cm)	1.89 ± 0.54 [1.63, 2.16]	2.36 ± 0.62 [2.06, 2.66]	24.7%	0.003	0.79
Displacement at 200ms (cm)	3.55 ± 0.88 [3.13, 3.98]	3.00 ± 1.02 [2.51, 3.49]	-15.5%	0.001	-0.89
Path Length (cm)	6.17 ± 1.43 [5.48, 6.86]	6.30 ± 1.36 [5.64, 6.95]	2.1%	0.611	0.12
Head excursion relative to the torso					
Peak (cm)	11.31 ± 3.32 [9.71, 12.91]	7.21 ± 3.15 [5.69, 8.72]	-36.3%	<0.001	-1.35
At 100 ms (cm)	8.22 ± 1.53 [7.48, 8.96]	5.13 ± 1.34 [4.48, 5.78]	-37.6%	<0.001	-1.66
At 200 ms (cm)	9.72 ± 2.30 [8.62, 10.83]	6.08 ± 2.14 [5.05, 7.11]	-37.5%	<0.001	-1.67
Time lag between head and torso peak values					
Displacement (ms)	71.9 ± 67.6 [39.3, 104.5]	48.6 ± 79.6 [10.3, 87.0]	-32.4%	0.096	-0.40
Velocity (ms)	-88.2 ± 19.9 [-97.8, -78.6]	-65.6 ± 28.9 [-79.5, -51.6]	-25.7%	0.002	0.83

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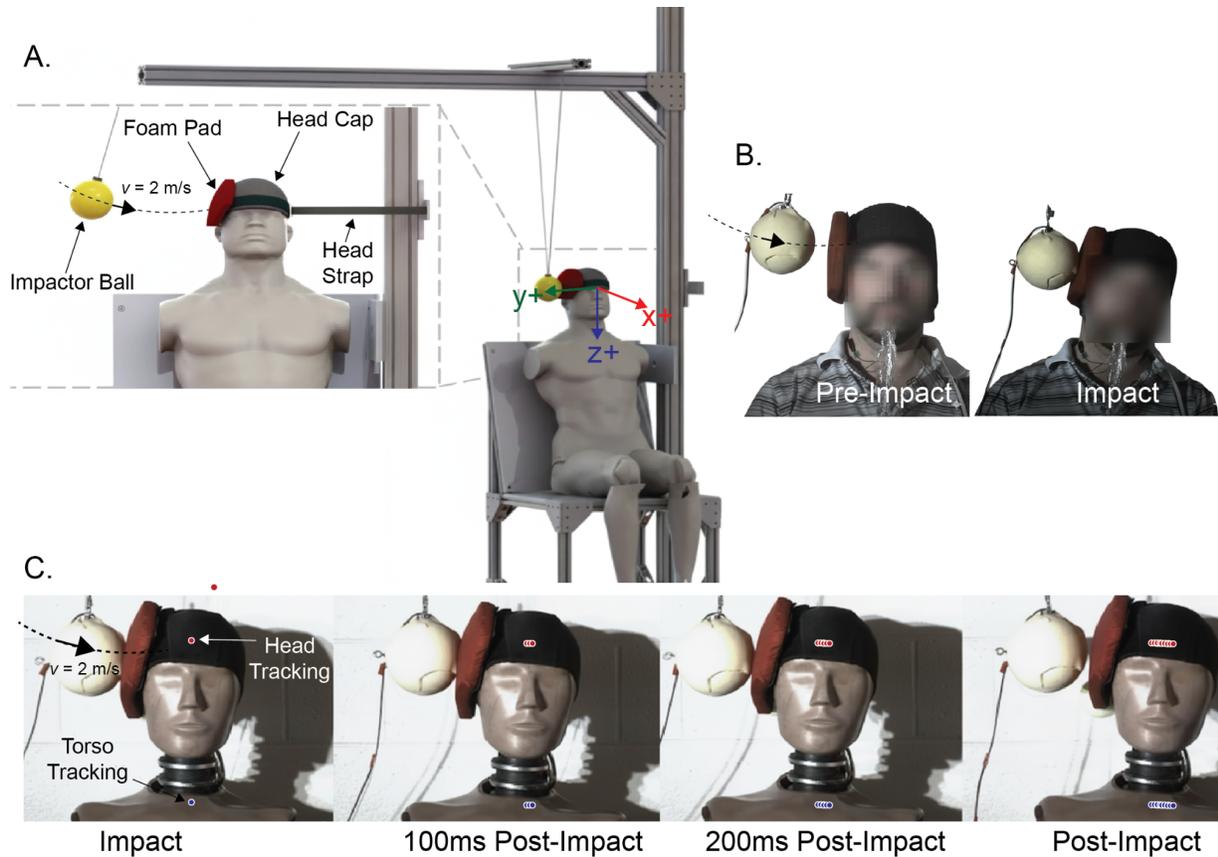
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473 **Table 3.** Peak kinematic parameters for head and torso (n = 19). Values are mean \pm SD [95% CI]. $\Delta\%$ =
 474 percent change from passive to co-contracted. Paired t-tests; Cohen's d effect size.

Parameter	Passive	Co-contraction	$\Delta\%$	p	d
Head					
Peak Velocity (cm/s)	149.7 \pm 11.2 [144.3, 155.0]	140.0 \pm 12.9 [133.8, 146.3]	-6.4%	0.003	-0.78
Peak Acceleration (g)	10.28 \pm 0.87 [9.86, 10.70]	10.13 \pm 1.04 [9.62, 10.63]	-1.5%	0.415	-0.19
Peak Angular Velocity (rad/s)	4.29 \pm 0.98 [3.82, 4.77]	4.05 \pm 0.90 [3.62, 4.49]	-5.6%	0.320	-0.23
Peak Angular Acceleration (rad/s ²)	280 \pm 67 [247, 312]	276 \pm 64 [245, 307]	-1.3%	0.820	-0.05
Torso					
Peak Velocity (cm/s)	43.6 \pm 11.0 [38.3, 48.9]	44.1 \pm 12.5 [38.1, 50.2]	1.2%	0.865	0.04
Peak Acceleration (g)	2.29 \pm 1.28 [1.67, 2.90]	2.19 \pm 0.81 [1.80, 2.59]	-4.1%	0.713	-0.09

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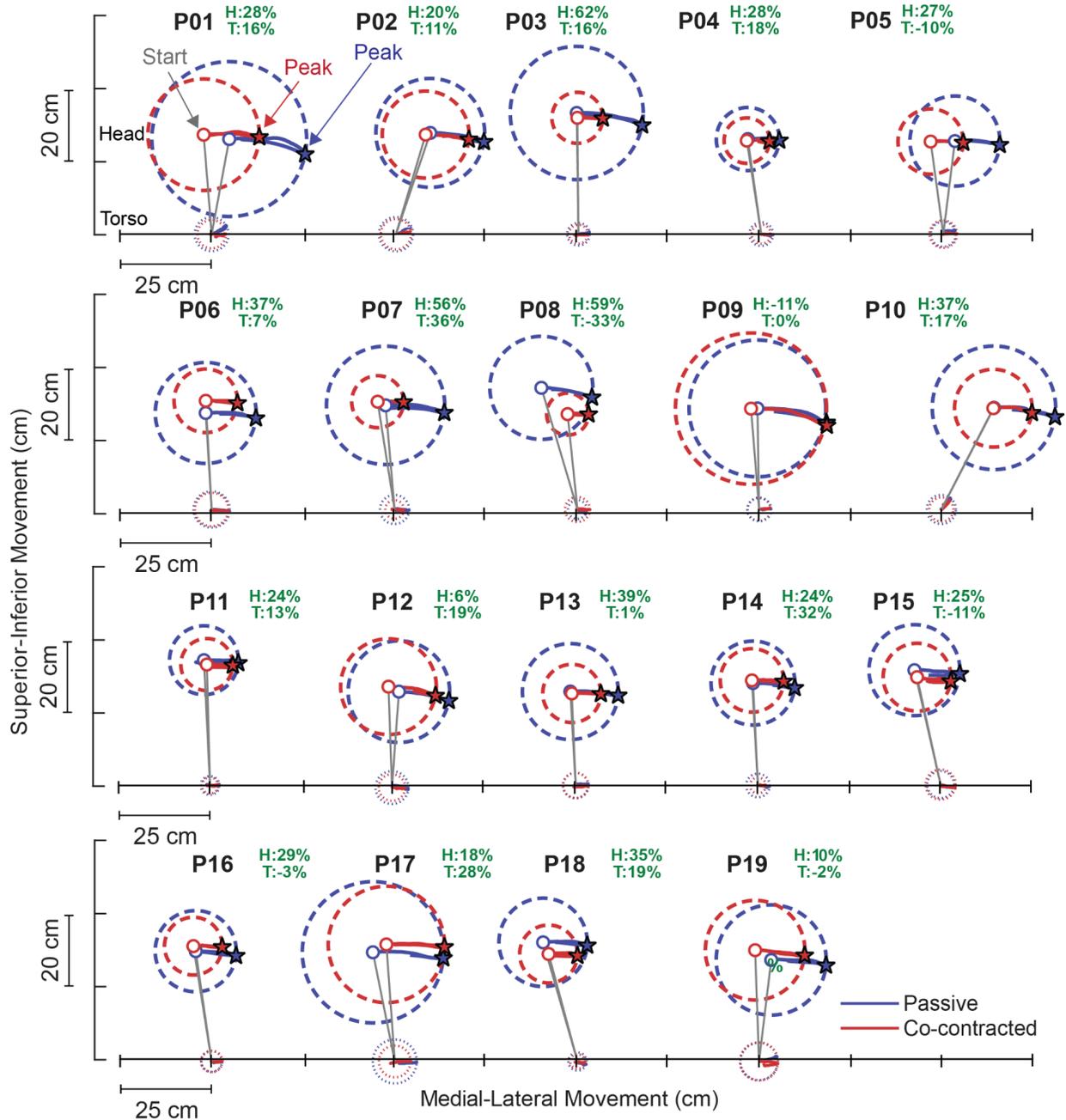
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478 **Figure 1.** Experimental setup and video digitization method. (A) Bi-filament pendulum system delivering
 479 2.0 m/s lateral impacts from a 3.7 kg padded impactor to a location 75 mm above the right tragus. High-
 480 speed cameras recorded at 500 Hz. (B) Representative impact sequence showing pre-impact positioning
 481 (left) and padded impactor contact (right). (C) Frame-by-frame digitization of head (red dot on protective
 482 cap) and torso (blue dot in upper cervicothoracic region) positions using Tracker software (Open-Source
 483 Physics, v6.2.0). An anthropomorphic test dummy demonstrates the digitization method for clarity.

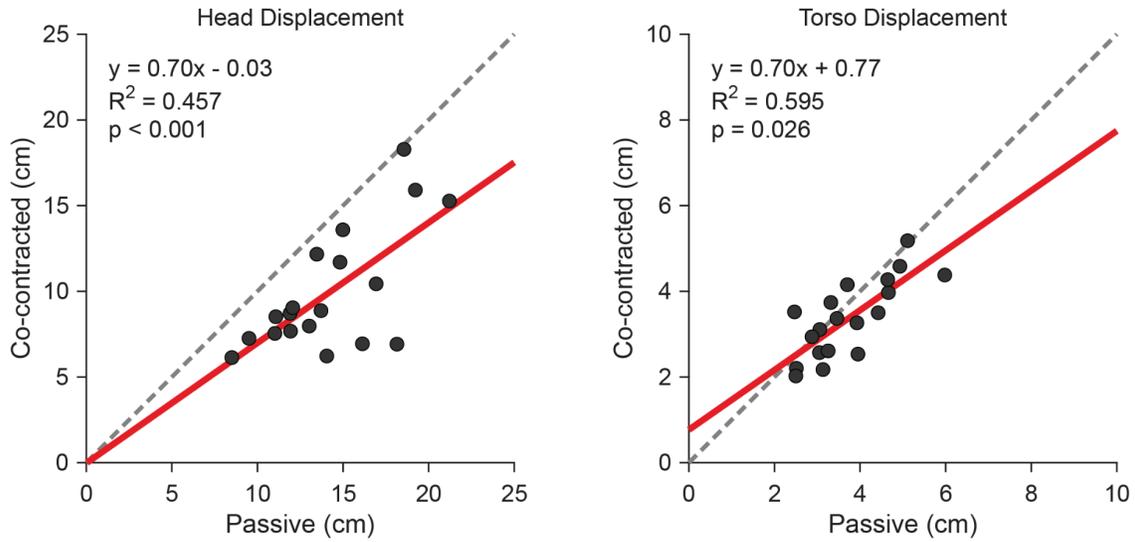
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486 **Figure 2.** Individual head and torso trajectories during lateral impact ($n = 19$). Movement paths in the
 487 medial-lateral and superior-inferior plane under passive (blue) and co-contracted (red) conditions, aligned
 488 to torso starting position. Solid lines trace movement from initial position (circles) to peak displacement
 489 (stars). Dashed circles indicate peak displacement magnitude. Green percentages show head (H) and torso
 490 (T) displacement reductions with co-contraction; negative values indicate increased displacement. Gray
 491 lines connect head and torso starting positions.

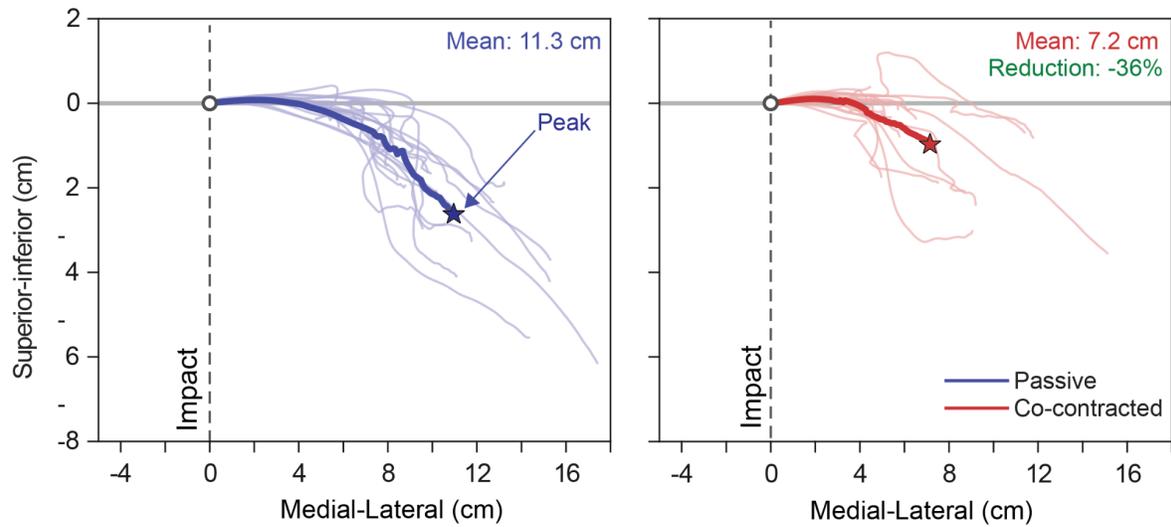
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494 **Figure 3.** Individual participant displacement responses in passive versus co-contracted conditions (n =
 495 19). Peak head displacement (left) and peak torso displacement (right). Gray dashed line indicates equality
 496 between conditions; red line shows linear regression fit. Points below the equality line indicate reduced
 497 displacement with co-contraction. Regression equations and R^2 values appear in each panel.

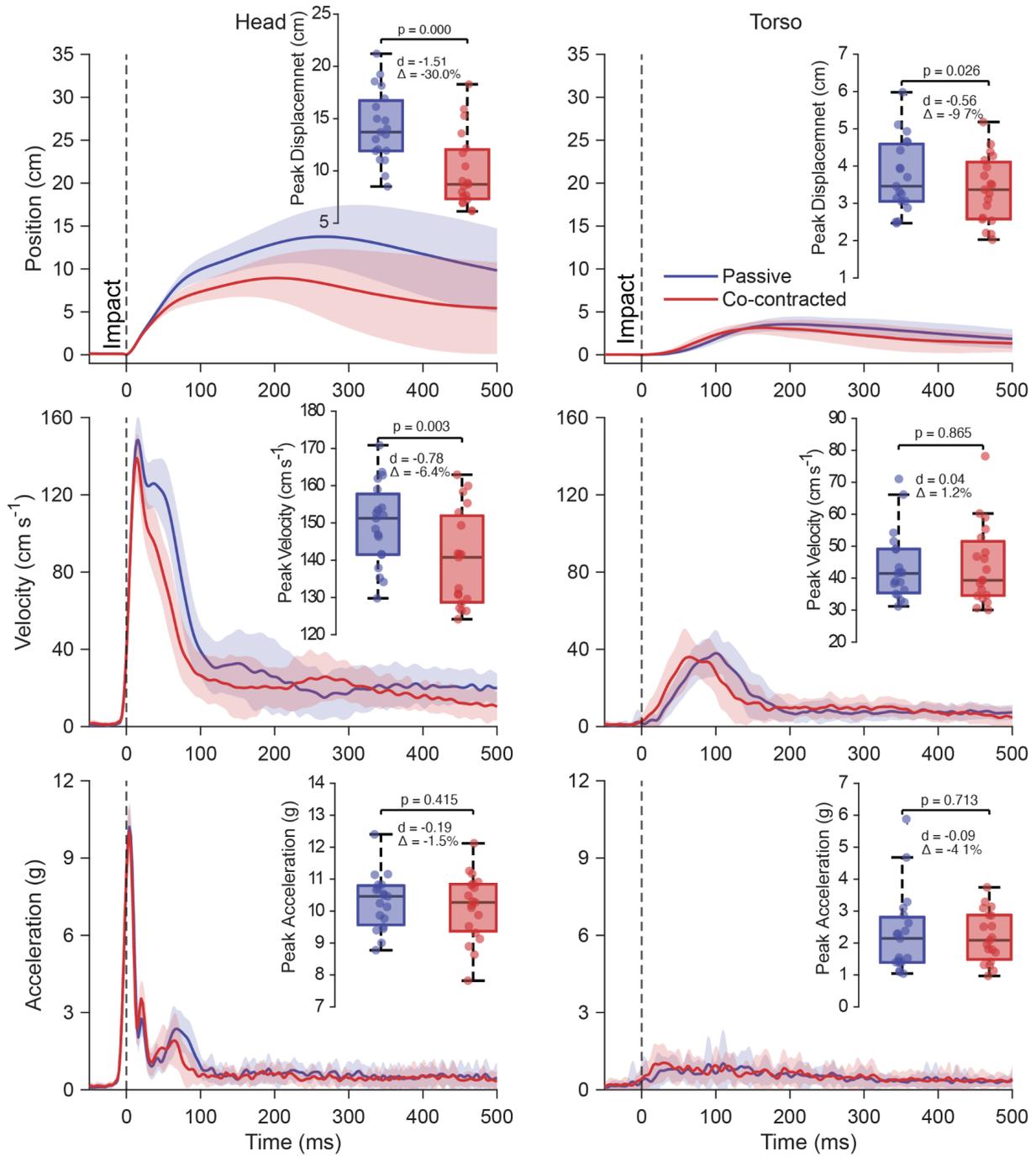
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500 **Figure 4.** Head position relative to torso during lateral impact (n = 19). Movement paths in the medial-
 501 lateral and superior-inferior plane, aligned to starting position (0, 0) and truncated at peak excursion.
 502 Passive (left, blue) and co-contracted (right, red) conditions show individual trajectories (light lines) and
 503 mean trajectory (dark line). Circles mark initial position; stars mark mean peak excursion.
 504

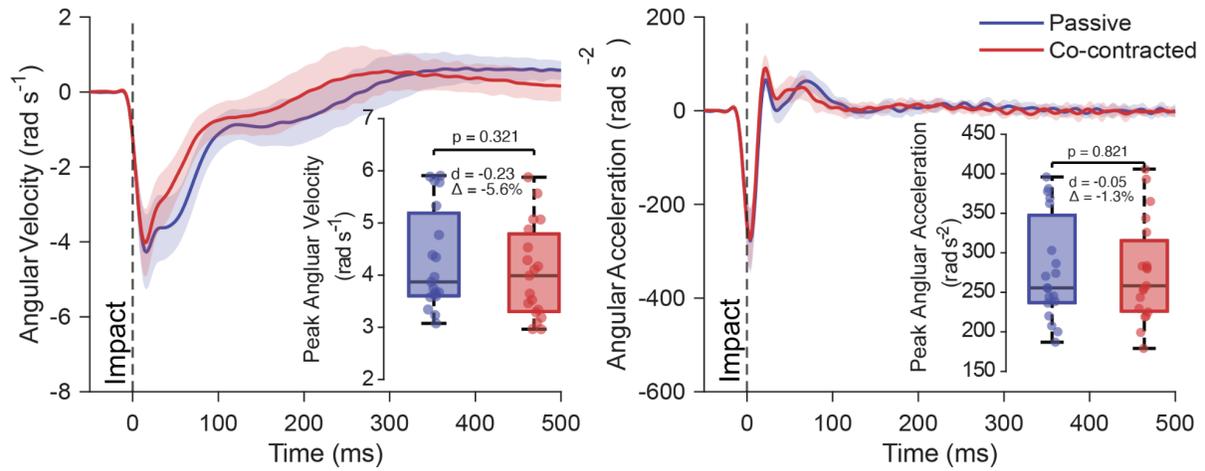
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507 **Figure 5.** Head and torso kinematics during lateral impacts (n = 19). Position (top), velocity (middle), and
 508 acceleration (bottom) for head (left) and torso (right) in passive (blue) and co-contracted (red) conditions.
 509 Solid lines represent means; shaded regions represent ±1 SD. Dashed vertical line marks impact onset (t =
 510 0 ms). Inset boxplots show peak values with individual data points, p-values, Cohen's d, and percent change.

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513 **Figure 6.** Head angular kinematics during lateral impacts (n = 19). Angular velocity (left) and angular
 514 acceleration (right) in passive (blue) and co-contracted (red) conditions. Solid lines represent means;
 515 shaded regions represent ± 1 SD. Dashed vertical line marks impact onset (t = 0 ms). Inset boxplots show
 516 peak values with individual data points, p-values, Cohen's d, and percent change.

517